High-speed impact across scales: a hybrid approach

Basilisk (and Gerris) Users' Meeting

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Introduction Group updates







Dr. Michael Negus (2022)

Dr. Ben Fudge (2023)

Some activities in the wider collaborative group:

Drop dynamics

- . Bouncing
- Coalescence
- Splashing
- Fluid-structure interaction





Acknowledgements:

EPSRC (EP/V051385/1 on liquid film control, EP/W032201/1 on ReproHacks) and NSF (EP/W016036/1) ٠

Liquid films

UK Fluids Network (Drop Dynamics and Interfacial Flows SIGs)







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Oscar Holrovd (2025)

Industrial mathematics Sustainable software Outreach and art

Sebastian Dooley (2026)





Multi-physics modelling

Asymptotic analysis

Equation discovery

Control theory



Throwback Thursday









End

Studying the dynamics of droplets in high speed flow conditions has ramifications particularly in the aeronautics industry, where the following flight conditions:

heavy rainfall

Motivation Background

high liquid water content (LWC) regions - clouds

are commonplace.

Ice formation severely affects aerodynamic performance. Of particular interest are the adverse effects on the nacelle system.







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Proposed new rulemaking by both EASA and the FAA is requiring water catch analysis to consider freezing rain and drizzle, which are characterized by water droplets of larger diameter than what are general considered for certification.

Task description:

- Blow-off factors for water catch are currently not well understood;
- required in the analysis of Nacelle ice protection system performance;
- would result in reduced bleed air off-take demand on the engine compressor, hence reduced fuel burn.



Primary objective: Using modelling, analysis and computational fluid dynamics (CFD) tools in order to study the rich dynamics of drop impact onto solid surfaces (including drop formation and pinch-off) within parameter ranges suitable from the physical standpoint.

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Single drop impact Droplet behaviour - summary - RC & Papageorgiou, IJMF 107, 192-2017 (2018)

Detailed analysis of splashing dynamics has been performed in both two and three dimensions, revealing similar qualitative and quantitative features.

- small drops: pancaking behaviour, no splashing;
- medium drops: deformation before impact, moderate splashing;
- ► large drops: stronger deformation, violent splashing;

 $d^* = 20 \ \mu m \qquad d^* = 200 \ \mu m \qquad d^* = 200 \ \mu m \qquad d^* = 2000 \ \mu$



 $\Lambda/\Delta R\Lambda$



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Pre-impact dynamics Experiments (NASA & INTA)



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During 2012 – 2015, Vargas, Sor and Magarino (NASA - INTA Madrid collaboration) have conducted a set of experiments on droplet breakup near the leading edge of an airfoil.



Figure 2.- Experiment set-up in the INTA test cell.

Pre-impact dynamics Experiments (NASA & INTA)

During 2012 – 2015, Vargas, Sor and Magarino (NASA - INTA Madrid collaboration) have conducted a set of experiments on droplet breakup near the leading edge of an airfoil.

Key observations:

- small drops tend to retain their shape;
- medium sized drops flatten into squashed ellipsoidal shapes;
- large drops eventually break under violent rupture.



Drop deformation and breakup as $D = 362 \ \mu m$ (above), D = 1130 μm (middle) and D = 2064 μm (below)



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Excellent qualitative agreement is found between the experiments and computations in the same parameter range, with good quantitative agreement also found in the proposed deformation rate metric.



With the aid of the simulations dynamics for much smaller drops is analysed, while also gathering break-up data in the timesteps just before impact.



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Impact Asymptotic structure - RC & M.R. Moore, JFM 856, 764-796 (2018)





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Impact Asymptotic structure - RC & M.R. Moore, JFM 856, 764-796 (2018)



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- Outer: boundary conditions linearise onto y = 0, solved using Riemann-Hilbert techniques.
- Inner ('jet-root'): quasi-steady Helmholtz flow, solved using Schwarz-Christoffel mappings.
- Jet: thin, high-speed jet governed by zero-gravity shallow-water equations, solved using characteristics.

Given time and patience, useful quantitative information about the impact process and properties of the resulting jet is retrieved:

Location of jet root:

$$\hat{x}_{j} = 2\sqrt{\frac{(1+V)R}{1+R}}\hat{t},$$

$$\hat{y}_{j} = \left(\frac{(3RV+R-V-3)}{2(1+R)}\hat{t}\right).$$

Jet thickness:

$$H_j(\hat{t}) = rac{\pi (1+V)^{3/2}}{8} \sqrt{rac{1+R}{R}} \hat{t}^{3/2},$$

Jet velocity:

$$U_j = 2\dot{\hat{d}}_0 = 2\sqrt{\frac{(1+V)R}{1+R}}\hat{t}^{-1/2},$$





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At early times we find excellent agreement between the two approaches. This begins to deteriorate (in an anticipated manner):

- at the tip of the jet;
- when not correcting for the presence of entrapped air bubbles;
- once we force the underlying assumptions (e.g. lower impact velocities);
- at sufficiently large times;





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From the inner region we can also derive the jet angle, found to be

$$\alpha = \delta^{1/2} \left((R-1) \sqrt{\frac{1+V}{R(1+R)}} \right) \sqrt{\hat{t}} + o(\delta^{1/2}),$$

where α is small. Abstractly it represents the slope of the vortex sheet in the outer region as it approaches the turnover point. R = 1, V = 2:



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The volumes of the satellite droplets in the system follow a log-normal distribution during most of the simulation, with an average area equal to roughly 1/10000 relative to the initial droplet. This behaviour is consistent with experimental observations (Mundo, *IJMF*, 95 and Yarin, *JFM*, 1995) for lower velocity impacts onto solid surfaces.



Droplet distribution for an $\theta = 60^{\circ}$ angle of incidence impact in the case of a range of droplet sizes.

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Post-impact dynamics Twin peaks - RC & Papageorgiou, IJMF 107, 192-2017 (2018)





The evolution of the drop size distribution hints at a separation in drop behaviour depending on size:

- the larger fluid volumes are found as spherical caps in contact with the solid surface
- are more likely to grow in time as coalescence events take place.
- the smaller drops are airborne and subjected to the strong background flow.
- tend to break up as long as capillary forces allow it.

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So ... what have we been up to since then?











We find that the perturbation to the free surface satisfies the singular integro-differential equation

$$0 = \frac{d\tilde{h}_0}{ds} + 2\kappa(s) + \frac{1}{2} \sum_{-\infty}^{\infty} \operatorname{cosech}\left(\frac{\pi(s-t)}{2}\right) \left[\tilde{h}_0(t)\kappa(t) - 2\kappa(t)\tilde{w}^*(t)\right] dt,$$

where $\tilde{w}^* = -2 \arctan\left(e^{\pi s/2}\right).$





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The effect of viscosity is to thicken the jet at the outlet by twice the angle the tangent to the free surface turns as *s* increases.

► the ratio of the jet thickness at the outlet (s = ∞) to that at the inlet (s = -∞) is given by

$$\frac{(H + \varepsilon^2 \tilde{h}_0)(\infty)}{(H + \varepsilon^2 \tilde{h}_0)(-\infty)} = 1 + \frac{\pi}{Re} + o\left(\frac{1}{Re}\right).$$





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• quantitatively, the free surface suffers a normal translation given by $\phi_1 = -\kappa x(y - 1/We)$.





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The key example is the (suitably scaled) leading-order-inner problem according to Wagner theory for a droplet-droplet impact at small times.



The dashed line indicates a dividing streamline that terminates at a relative stagnation point on the body at S. In a frame moving with the turnover points, the problem is a Helmholtz flow.



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- Downstream as s → ∞, one can see the perturbation approaching an analytically predicted value of −2π;
- Upstream we see inverse square-root decay back into the bulk (the outer Wagner region), displayed in further detail in the inset.



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Results Inner region - M.R. Moore, RC, Ock², J.M. Oliver, JFM 882, A19 (2020)



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End

Despite the problem being in 2D, numerically this is a challenge:

 initial and boundary conditions are implemented based on asymptotic expressions valid 'in the far-field';



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End

- initial and boundary conditions are implemented based on asymptotic expressions valid 'in the far-field';
- the underlying theory is powerful and valid up to second order



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End

- initial and boundary conditions are implemented based on asymptotic expressions valid 'in the far-field';
- the underlying theory is powerful and valid up to second order, but ...



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- initial and boundary conditions are implemented based on asymptotic expressions valid 'in the far-field';
- the underlying theory is powerful and valid up to second order, but ... it ignores the gas altogether, and it need not bother with contact angles, outflow conditions etc.



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- ▶ the higher the *Re*, the better the analytical predictions.



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- ► the higher the *Re*, the better the analytical predictions. The higher the *Re* ⇒ ill-conditioning and instabilities.



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- ► Any corrections/targets are of size 1/*Re*... in a restrictively large domain (*L* ≈ 200 here).



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A truly symbiotic relationship?





In the same spirit ... Levitating a cylinder - Dalwadi, RC et al., JFM 917, A28 (2021)

Direct numerical simulations can be deployed alongside beautiful matched asymptotic expansion methods for a wide class of problems as means to resolve complex physical systems with no fitting parameters, with experiments providing essential confirmation.





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Bringing it all together - a hybrid multi-scale framework









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End

For us to be able to get closer to an (accurate and efficiently obtained) answer, any solution would need to resolve:

- sub-micron scales on impact and for the fragmentation process.
- O(1) m or larger lengthscales for device-specific geometries.



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No monolithical solver could viably do this.



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 $\mathcal{O}(1\,\mu\mathrm{m}) - \mathcal{O}(1\,\mathrm{mm})$ (splashing dynamics) $\mathcal{O}(1\,\mathrm{mm}) - \mathcal{O}(10\,\mathrm{mm})$ (droplet cloud)

 $\mathcal{O}(10\,\mathrm{mm}) - \mathcal{O}(1\,\mathrm{m})$ (secondary drop trajectories)

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Conclusions Acknowledgements



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without which this work would not have been possible.





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